

# Thermal Decomposition of NF<sub>3</sub> with Various Oxides

Elizabeth Vileno,<sup>†</sup> Michael K. LeClair,<sup>‡</sup> Steven L. Suib,<sup>\*,†,‡,§</sup> Michael B. Cutlip,<sup>‡</sup>  
Francis S. Galasso,<sup>†</sup> and Steven J. Hardwick<sup>†</sup>

U-60, Department of Chemistry, Department of Chemical Engineering, and  
Institute of Material Sciences, University of Connecticut, Storrs, CT 06269-3060, and  
Ecosys, 7 Commerce Drive, Danbury, Connecticut 06810

Received October 17, 1995. Revised Manuscript Received March 19, 1996<sup>®</sup>

The thermal decomposition of NF<sub>3</sub> by various oxides was investigated using gas chromatography, BET surface areas, and X-ray powder diffraction. The decomposition of NF<sub>3</sub> using alumina can occur at temperatures as low as 100 °C, with steady complete conversion for almost 4 h at 400 °C. The reaction is shown to be stoichiometric. Using Na-doped alumina, conversion of NF<sub>3</sub> dropped off faster than conversion with the undoped alumina. Similarly, calcium oxide did not react with the NF<sub>3</sub> as completely or last as long as the alumina did; even at 400 °C the conversion of NF<sub>3</sub> was only briefly greater than 90%. HX zeolite was also reacted with NF<sub>3</sub>, with higher and more consistent conversion than occurred with calcium oxide and Na-doped alumina, but did not perform as well as the alumina. Over 98% conversion was maintained at 400 °C for more than 1 h. In all cases, nitrogen oxides and the corresponding metal fluorides were the only major products from the reactions. The XRD patterns confirm the presence of metal fluorides for all of the materials investigated. On the basis of these investigations, it has been concluded that of all the oxides studied, alumina is the best oxide getter for NF<sub>3</sub>.

## Introduction

In the past decade, the use of NF<sub>3</sub> has increased dramatically. This is primarily due to the development of NF<sub>3</sub> as an etching and cleaning agent in the semiconductor industry. The development of a plasma method that can enhance reaction selectivity while at the same time reduce damage and contamination has become increasingly important as the sophistication of integrated circuit technology has increased. NF<sub>3</sub> has managed to fill this role.

NF<sub>3</sub> plasmas for cleaning and etching have several advantages over the more commonly used CF<sub>4</sub> plasmas. NF<sub>3</sub> is easily stored and handled at ambient conditions. It leaves no carbonaceous residue behind; the byproducts are gaseous,<sup>1</sup> consisting mostly of N<sub>2</sub>, O<sub>2</sub>, NO<sub>x</sub>'s, and the corresponding fluoride (such as SiF<sub>4</sub> when cleaning Si-containing materials). In addition, etch rates for NF<sub>3</sub> are considerably faster than those for CF<sub>4</sub>. For example, a 20% NF<sub>3</sub> (balance Ar) mixture had a Si etch rate 10 times faster than pure CF<sub>4</sub> and 3 times faster than a 4% oxygen (balance CF<sub>4</sub>) mixture. Selectivities for silicon over silicon dioxide have been reported as high as 50:1.<sup>1</sup> Also, oxygen can be mixed with NF<sub>3</sub> to increase the oxygenation rate of silicon,<sup>2</sup> or hydrogen with NF<sub>3</sub> to improve etching selectivity of SiO<sub>2</sub> with respect to Si.<sup>3</sup>

NF<sub>3</sub> has been found to be an excellent choice for cleaning many commonly used semiconductor materials

such as silicon,<sup>1,4,5</sup> tungsten,<sup>6</sup> and tungsten silicide,<sup>7</sup> as well as other materials. It can also be used for cleaning reactor chambers<sup>8</sup> and reactors<sup>9</sup> without leaving unwanted residue behind.

Two of the biggest concerns in using NF<sub>3</sub> is its cost and toxicity. NF<sub>3</sub> costs more than CF<sub>4</sub> and is more toxic. The threshold limit value is 10 ppm; higher chronic doses can cause liver and kidney damage, and an acute high dosage could cause poisoning from anoxic death.<sup>10</sup> Two other concerns are its effect as a greenhouse gas because of a very long atmospheric lifetime and its explosive reactivity toward metal hydrides. Because of these concerns, new processes need to be developed to destroy or remove unreacted effluent NF<sub>3</sub>.

Several types of scrubbers are currently used to trap or decompose NF<sub>3</sub>. Incineration (with and without hydrocarbon fuels) is one of the more popular methods used. This results in NO<sub>x</sub> and HF production. Activated carbon scrubbers are also used, but there are concerns of accidental NF<sub>3</sub> releases or decomposition to volatile fluorocarbons.<sup>1,4,11</sup> Aqueous scrubbers have never been tried because of the very slow hydrolysis of NF<sub>3</sub> and its low solubility in water.<sup>12</sup>

(3) Yokoyama, S.; Yamakage, Y.; Hirose, M. *Appl. Phys. Lett.* **1985**, *47*, 389–91.

(4) Barkanic, J.; Hardy, T.; Shay, R. H.; Fukushima, H. Off-gas analysis and disposal of NF<sub>3</sub> in plasma processing; Air Products and Chemicals, Inc., Allentown, PA; and Daido Sanso KK, Osaka, Japan, 1984.

(5) Delfino, M.; Chung, B. C.; Tsai, W.; Salimian, S.; Favreau, D. P.; Merchant, S. M. *J. Appl. Phys.* **1992**, *72*, 3718–25.

(6) Hirase, I.; Petitjean, M. European Patent *EP 382,986*, 1990.

(7) Lee, R.; Terry, F. L. *J. Vac. Sci. Technol. B* **1991**, *9*, 2747–51.

(8) Langan, J. G.; Felker, B. S. In *Proceedings Electrochemical Society*, 1992; pp 135–44.

(9) Bruno, G.; Capezzuto, P.; Cicala, G.; Manodoro, P. *J. Vac. Sci. Technol. A* **1994**, *12*, 690–8.

(10) Schaefer, J.; Otsuka, A. Alternative Nitrogen Trifluoride Abatement System: Matheson Electronic Products Group, San Jose, CA.

(11) Aramaki, M.; Nakagawa, S.; Nakano, H.; Ichimaru, H.; Tainake, M. Ger. Offen. DE 4,002,642, 1990.

<sup>†</sup> Department of Chemistry.

<sup>‡</sup> Department of Chemical Engineering.

<sup>§</sup> Institute of Material Sciences.

<sup>†</sup> Ecosys.

\* To whom correspondence should be addressed.

® Abstract published in *Advance ACS Abstracts*, May 1, 1996.

(1) Woytek, A.; Lileck, J. T.; Barkanic, J. A. *Solid State Technol.* **1984**, *72*, 172–5.

(2) Morita, M.; Kubo, T.; Ishihara, T.; Hirose, M. *Appl. Phys. Lett.* **1984**, *45*, 1312–14.

**Table 1. BET Surface Area Measurements of the Various Oxides before Being Reacted with NF<sub>3</sub>**

oxide	S.A. (m <sup>2</sup> /g)
alumina	330
Na-doped alumina	233
calcium oxide	<5
HX zeolite	155

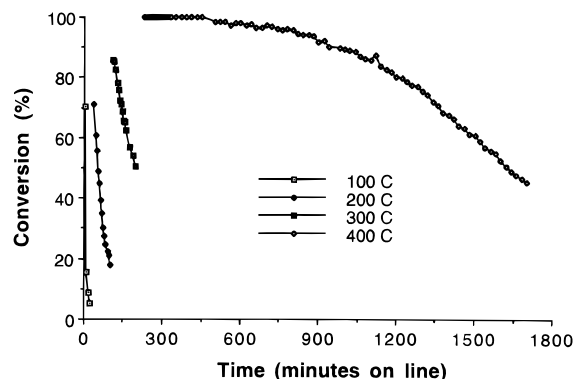
Some systems have been reported that use metals, supported metals, and oxides to thermally decompose NF<sub>3</sub> to nitrogen (or nitrogen oxides for oxide materials) and the corresponding fluorides. For example, consider the following patents: BN at 250–260 °C;<sup>13,14</sup> Si<sub>3</sub>N<sub>4</sub> at ≥200 °C;<sup>15</sup> Cu and Ni non-oxide compounds supported on activated carbon at 100–300 °C;<sup>16</sup> and metal oxides and activated carbon at 200–600 °C.<sup>17</sup> Pure metal and metalloid systems have also been suggested, Ti was used at temperatures ≥200 °C,<sup>18</sup> and Si, B, W, Mo, V, Se, Te, Ge, and/or their non-oxide compounds was used to decompose NF<sub>3</sub> at temperatures between 200 and 800 °C.<sup>19</sup>

However, to choose an optimum getter for NF<sub>3</sub>, a systematic comparison of the effectiveness of various materials is in order. In an earlier paper, we considered thermal decomposition by various metals.<sup>20</sup> The research presented here is concerned with the thermal decomposition of NF<sub>3</sub> using Al<sub>2</sub>O<sub>3</sub>, Na-doped Al<sub>2</sub>O<sub>3</sub>, CaO, and HX zeolite. Surface area measurements and X-ray diffraction were used to help explain the decomposition process, with the objective of finding the material that can consistently decompose NF<sub>3</sub> at the lowest possible temperature.

## Experimental Section

**Materials and Preparation.** NF<sub>3</sub> (1% by mol, balance He) was purchased from Air Products and Chemicals in Allentown, PA. The following oxides were used after heating to 450 °C for 2 h in flowing He and were obtained from the following sources:  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, crushed with fines removed, from La Roche Chemicals, Baton Rouge, LA; Na doped  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>, crushed with fines removed, from La Roche Chemicals, Baton Rouge LA; and CaO, reagent grade, pressed into a pellet, then crushed with fines removed, from Allied Chemical Co., Morristown, NJ. HX zeolite was prepared from NaX zeolite by ion exchange with NH<sub>4</sub>NO<sub>3</sub> overnight twice, and then heated to 375 °C for 12 h. It was then pressed into a pellet, crushed with fines removed, and heated to 350 °C for 2 h in flowing He. The NaX zeolite was purchased from Alfa Products, in Danvers, MA, and the NH<sub>4</sub>NO<sub>3</sub> from J.T. Bakers, Phillipsburg, NJ. Ultra high-purity grade He gas was purchased from Aero All-Gas Co., in Hartford, CT.

**Reaction Process.** The reactions involved successive heating of the oxide materials to four different temperatures, 100, 200, 300, and 400 °C. Approximately 0.350 g of material was placed inside a reactor made of 1/8 in. Inconel tubing

**Figure 1.** Conversion results for alumina.**Table 2. Summary of the Initial Conversion of NF<sub>3</sub> by the Various Oxides Investigated**

oxide	initial conversion (% of NF <sub>3</sub> ) (minutes conversion was maintained)			
	100 °C	200 °C	300 °C	400 °C
alumina	70	71	86	100 (222 min)
Na-doped alumina	15	57	90	98 (20 min)
calcium oxide	>2	2	29	92
HX zeolite	>2	17	100 (<7 min)	>98 (91 min)

plugged with glass wool. The materials were heated for 2 h at 450 °C (HX zeolite at 350 °C) in flowing He to drive off any water. Nitrogen trifluoride (1%) was passed over the oxide at a flow rate of 7.5 mL/min after the sample had equilibrated at the chosen temperature. The residence time was calculated to be about 0.2 s. Gas chromatograph analyses were done at approximately 7 min intervals. A tube furnace was used to heat the vertically placed reactor, and the thermocouple was placed in the reactor directly above the bed of oxide. See the reactor design description in a previous paper.<sup>20</sup>

The gas chromatograph used was a Hewlett-Packard 5890 Series II gas chromatograph equipped with a thermal conductivity detector and an HP 3396 Series II integrator. A Haysep D packed column was used to separate the gases. The system can detect NF<sub>3</sub> to less than 0.002 mol % in the exhaust gas. The percent conversion of NF<sub>3</sub> was calculated based on an average of NF<sub>3</sub> counts obtained by bypassing the reactor.

**Sample Characterization.** A Scintag XDS 2000 X-ray powder diffractometer was used to identify and characterize the reacted and unreacted materials. Cu K $\alpha$  radiation was used as the X-ray source, with a beam current and voltage of 45 mA and 40 kV, respectively. All patterns were compared to a JCPDS data base. Surface area measurements were done by BET, using an Omnisorp 100CX instrument with N<sub>2</sub> adsorption.

## Results

**Alumina.** A 0.350 g sample of alumina, with a BET surface area of 330 m<sup>2</sup>/g (see Table 1 for summary of BET surface areas before reaction), was heated in flowing He at 450 °C for 2 h, and then reacted with NF<sub>3</sub> at four different temperatures. Similar samples were heated under the same conditions, with a resulting 10% loss in mass, presumably from adsorbed water. Figure 1 shows the conversion results, and Table 2 summarizes all of the conversion results for the various oxides used. At 100 °C the conversion of NF<sub>3</sub> starts at 70%, but drops to 5% in 16 min. At 200 °C the conversion starts at 71% and drops to 18% in 42 min. At 300 °C conversion of 86% is reached initially, and by 87 min the conversion has dropped to 50%. Finally at 400 °C 100% conversion

(12) *Handbook of Chemistry and Physics*, 73rd ed.; CRC Press: Boca Raton, FL, 1992–1993; pp 79.

(13) Iwanaga, T.; Harada, I.; Aritsuka, M. Jpn. Kokai Tokkyo Koho JP 02,245,223, 1990.

(14) Iwanaga, T.; Harada, I.; Aritsuka, M. Jpn. Kokai Tokkyo Koho JP 02,265,6205, 1990.

(15) Kashiwada, K.; Hasumoto, T.; Torisu, J.; Konishi, M. Jpn. Kokai Tokkyo Koho JP 04,225,818, 1992.

(16) Kubo, M.; Nakagawa, S. Jpn. Kokai Tokkyo Koho JP 05,192,538, 1993.

(17) Orihara, I.; Fukushima, M.; Sato, S. Jpn. Kokai Tokkyo Koho JP 05,15,740, 1993.

(18) Katamura, K.; Sugano, K.; Nakayama, H. Jpn. Kokai Tokkyo Koho JP 61,287,424, 1986.

(19) Aramaki, M.; Sakaguchi, H.; Suenaga, T.; Kobayash, Y. Jpn. Kokai Tokkyo Koho JP 61,204,025, 1986.

(20) Vileno, E.; LeClair, M. K.; Suib, S. L.; Cutlip, M.; Galasso, F. S.; Hardwick, S. J. *Chem. Mater.* **1995**, 7, 683–687.

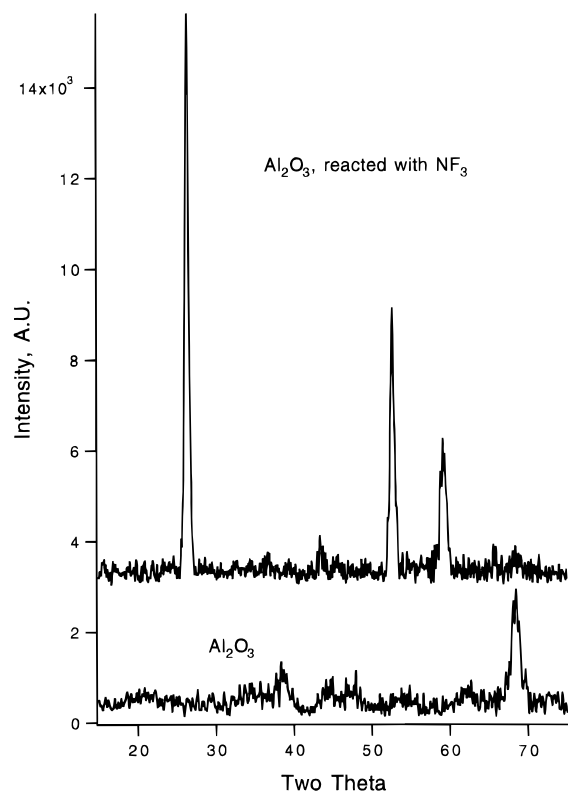


Figure 2. X-ray diffraction pattern for reacted alumina.

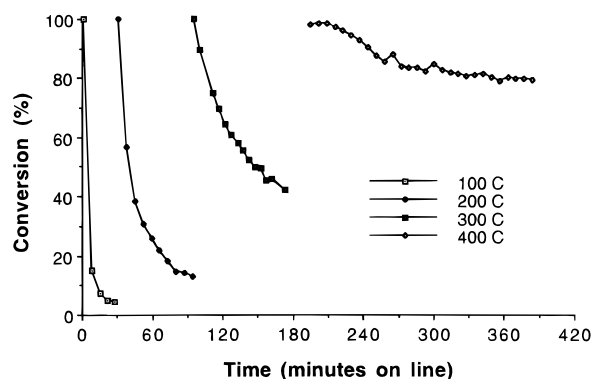


Figure 3. Conversion results for Na-doped alumina.

is reached and maintained for 222 min, and then drops to 50% at 1622 min on line, (for a total of 1392 min at 400 °C).

Major gaseous products are nitrogen oxides. After reaction the alumina sample weighed 0.460 g, for a net gain of 0.110 g. XRD results suggest that the unreacted alumina was mostly amorphous, with a broad low peak around 1.4 Å, as expected for  $\gamma$ -alumina. After reaction, an XRD pattern corresponding to  $AlF_3$  was detected. Figure 2 shows these XRD patterns.

**Na-Doped Alumina.** A 0.359 g sample of Na-doped alumina (8%  $Na_2O$  by mass), with a BET surface area of 233  $m^2/g$ , was reacted with  $NF_3$  under conditions similar to those for alumina. Figure 3 shows the results of  $NF_3$  conversion. At 100 °C the initial (highest) conversion of  $NF_3$  is 15%, dropping to 4% within 20 min. At 200 °C, the Na-doped alumina converts  $NF_3$  initially at 57%, and conversion drops to 13% within 56 min.  $NF_3$  conversion starts at 90% at 300 °C, and drops to 42% 91.5 min later. Finally, at 400 °C, conversions close to 100% are obtained but maintained for only 20 min, with

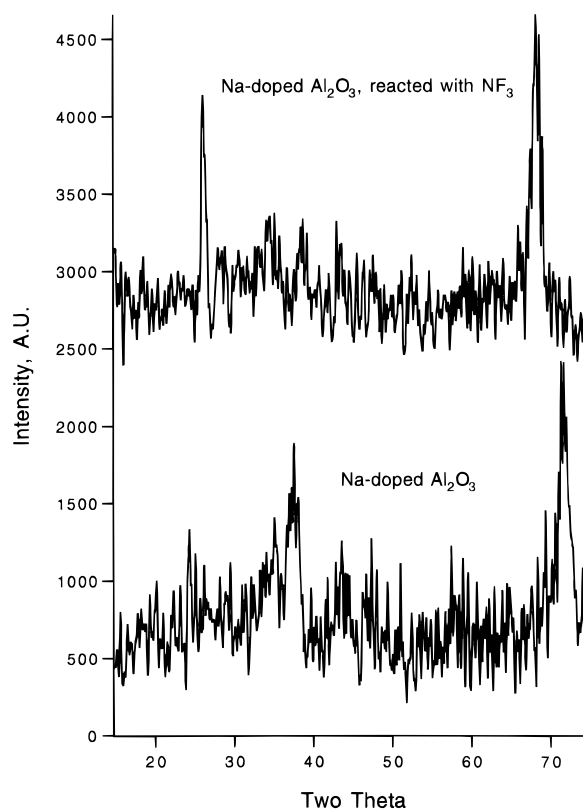


Figure 4. X-ray diffraction pattern for reacted Na-doped alumina.

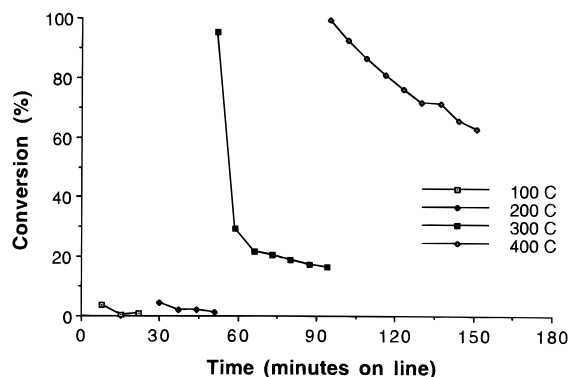


Figure 5. Conversion results for calcium oxide.

conversion dropping and leveling off at 80% for at least 90 min.

The XRD pattern of Na doped alumina before reaction was similar to the nondoped materials with a broad peak at 1.4 Å. After reaction, the main peak of  $AlF_3$  can be seen, but no peaks for  $NaF$  are evident. Figure 4 shows these XRD data.

**Calcium Oxide.** A 0.280 g sample of  $CaO$  was also reacted with  $NF_3$  (see Figure 5 for conversion results). The BET surface area was calculated to be less than 5  $m^2/g$ . At 100 °C, there was no significant (>2%) conversion. At 200 °C, the conversions obtained were very low, being about 2% for 14 min. At 300 °C, 29% conversion of  $NF_3$  was obtained. Conversion dropped quickly to 16% after 35 min. At 400 °C conversion started initially at 92% and dropped to 63% after 50 min.

The XRD patterns revealed that the only crystalline material before heating and reacting the  $CaO$  is  $Ca(OH)_2$ . After reaction the patterns for  $CaO$ ,  $Ca(OH)_2$ ,

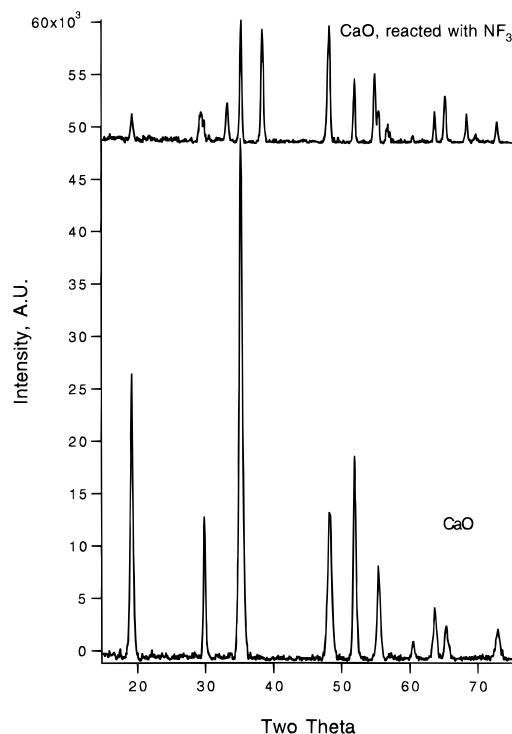


Figure 6. X-ray diffraction pattern for reacted calcium oxide.

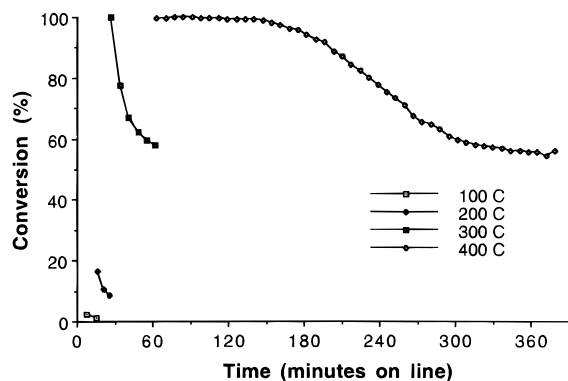


Figure 7. Conversion results for HX zeolite.

and  $\text{CaF}_2$  were all observed (see Figure 6 for XRD results).

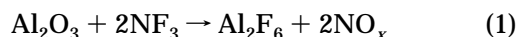
**HX Zeolite.** A 0.342 g sample of HX zeolite, with a BET surface area of  $155 \text{ m}^2/\text{g}$ , was reacted with  $\text{NF}_3$ . At  $100^\circ\text{C}$  there was no significant conversion. At  $200^\circ\text{C}$  the initial and highest conversion was 17%, dropping to 8.6% 10 min later. At  $300^\circ\text{C}$  there was 100% conversion, which immediately began dropping, decreasing to 58% about 35 min later. High conversions (>98%) were obtained at  $400^\circ\text{C}$  for 91 min. Conversion leveled off at 56% at 329 min, and the reaction was terminated at 379 min. Figure 7 shows the conversion results. XRD revealed the presence of amorphous material as a result of the reaction.

## Discussion

**Alumina Getters.** The alumina decomposed  $\text{NF}_3$  at  $100^\circ\text{C}$ . However, sustained 100% conversion was not achieved until the temperature was raised to  $400^\circ\text{C}$ . At this temperature the alumina was able to maintain 100% conversion for over 3.5 h. The instantaneous conversion of  $\text{NF}_3$  was plotted as a function of time. By integrating the curve, it was found that 68% of the  $\text{NF}_3$

passed over the getter was decomposed. The alumina was weighed before and after reaction with  $\text{NF}_3$ . Assuming a 10% loss in mass due to water (as other alumina samples had shown), the mass increased 146%, from 0.315 g to 0.460 g. The theoretical increase (100% conversion of alumina to  $\text{Al}_2\text{F}_6$ ) is a 165% mass increase. Therefore, 146% mass increase represents a 70% conversion of alumina to  $\text{Al}_2\text{F}_6$ , assuming it is the only solid product.

Several factors back up this assumption. No fluorinated gaseous or liquid components were detected in the exit stream, except for  $\text{NF}_3$ .  $\text{Al}_2\text{F}_6$  is seen as the only crystalline product using XRD. Thermodynamically,  $\text{Al}_2\text{F}_6$  is the expected product along with nitrogen oxide gases. Given this assumption, the close agreement of the  $\text{NF}_3$  conversion, and the selectivity to  $\text{Al}_2\text{F}_6$ , it is thought that the overall reaction is as follows:



$\text{NO}_x$ 's,  $\text{N}_2$ , and  $\text{O}_2$  gases are detected with GC experiments. However, the column used decomposes  $\text{NO}_x$  gases. It is therefore not possible to determine specific concentrations of the  $\text{NO}_x$ 's in the exit gas.

The reaction was terminated as the conversion of  $\text{NF}_3$  fell below 50%. It is believed that the process becomes increasingly mass transfer limited as more and more  $\text{Al}_2\text{F}_6$  is present.

**Na-Doped Alumina Getters.** Na-doped alumina was tried, with the expectation that NaF would be formed, as well as  $\text{Al}_2\text{F}_6$ . The surface area of this alumina was lower than that of the undoped material ( $233 \text{ m}^2/\text{g}$  as compared to  $330 \text{ m}^2/\text{g}$  for the undoped material), but this cannot account for the much lower activity. At  $400^\circ\text{C}$ , 100% conversion was never achieved, with 98% conversion holding steady for only 20 minutes. The lower activity could be due to pore blockage by the Na, resulting in severe mass-transfer effects. It is possible that the Na was active in decomposing  $\text{NF}_3$ , forming highly dispersed NaF, which may not be seen with XRD. The major peaks for  $\text{Al}_2\text{F}_6$  are present, indicating, as with the pure alumina, that aluminum sites play a major role in the decomposition of  $\text{NF}_3$ .

**CaO Getters.** A low surface area calcium oxide (lime) was chosen as a getter. It was thought that the stable and nontoxic  $\text{CaF}_2$  salt would be a desirable product. Also, lime is very inexpensive and handled easily. Unfortunately, although active initially, CaO was quickly deactivated. Probably as a result of the low surface area, mass transfer effects were greatly exaggerated, and even at  $400^\circ\text{C}$  there was not 100% conversion. The XRD confirms the presence of  $\text{CaF}_2$  after reaction, and the GC shows the production of  $\text{NO}_x$ 's.

**HX Zeolite Getters.**  $\text{NH}_4\text{X}$  zeolite was heated at  $350^\circ\text{C}$  to produce HX zeolite. HX was chosen because it has the highest Al:Si ratio of the common faujasitic zeolites, and previous work has shown that aluminum oxides are more active than silicon oxides in decomposing  $\text{NF}_3$ . Like the other oxides, there was no sustained activity at  $300^\circ\text{C}$  or below. At  $400^\circ\text{C}$  the zeolite decomposed  $\text{NF}_3$  for more than 60 min, making it a better getter than the Na-doped alumina, but not as efficient as the pure alumina. One interesting observation is that the XRD data showed no signs of  $\text{Al}_2\text{F}_6$  formation, and in fact it was amorphous (HX zeolite

decomposes at 400 °C).  $\text{NO}_x$ 's were detected as the major gaseous products.

### Conclusion

The general reaction of  $\text{NF}_3$  with oxides produces metal fluorides, unidentified  $\text{NO}_x$ 's, and possibly  $\text{N}_2$  and/or  $\text{O}_2$ . No  $\text{N}_2\text{F}_4$  was detected, despite measures to ensure detection. Activity of the oxides differed considerably, with mass-transport problems appearing to be the major cause of deactivation. Alumina and HX zeolite performed well, but the same alumina doped with Na (8%) and CaO were not as active. It is believed that high surface area may be an important factor in the activity of a particular compound but that the chemical species chosen is more important. For example, in several studies of different silicon oxides<sup>21</sup> it was found that varying the surface area of the silicon oxide from that of a typical quartz tube to  $>300 \text{ m}^2/\text{g}$  produced the same conversion results.

Table 3 compares the reactivity of  $\text{NF}_3$  with metals and oxides studied previously.<sup>20,22</sup> As can be seen, sustained 100% conversion using any material does not occur until temperatures over 300 °C have been reached. It is believed that the dissociation of  $\text{NF}_3$  (which

**Table 3. Comparison of the Activity for Various Oxides and Metals**

material	% conv at 300 °C	% conv at 400 °C	ref
silicon	50	100	20
titanium	80	100	20
zirconium	20	100	22
$\text{SiO}_2$	2	89 <sup>a</sup>	22
$\text{Al}_2\text{O}_3$	85 <sup>a</sup>	100	this work
Na-doped $\text{Al}_2\text{O}_3$	95 <sup>a</sup>	100 <sup>a</sup>	this work
CaO	95 <sup>a</sup>	100 <sup>a</sup>	this work
HX zeolite	100 <sup>a</sup>	100	this work

<sup>a</sup> Unsustained conversion (<10 min).

produces  $\text{NF}_2$  radicals and becomes significant above 300 °C) is involved in the decomposition of  $\text{NF}_3$ . This could help explain the rapid drop in conversion at lower temperatures. Also, mass-transfer effects may be more significant at the lower temperatures, especially given the quick residence time of 0.2 s.

**Acknowledgment.** Support for this research was from the Environmental Protection Agency administered through the Pollution Prevention Research and Development Center of the Environmental Research Institute at the University of Connecticut. We thank Jung Chou Lin for the BET surface area analysis.

CM9504955

(21) Vileno, E.; Suib, S. L., unpublished results, 1995.

(22) Vileno, E.; LeClair, M. K.; Suib, S. L.; Cutlip, M. In *Hazardous Waste Management Technologies*; Atlanta, GA, 1994.